

ECERTA PROJECT

**Computational Aeroelasticity
based on
Bifurcation Theory**

Sebastian Timme

Kenneth J. Badcock



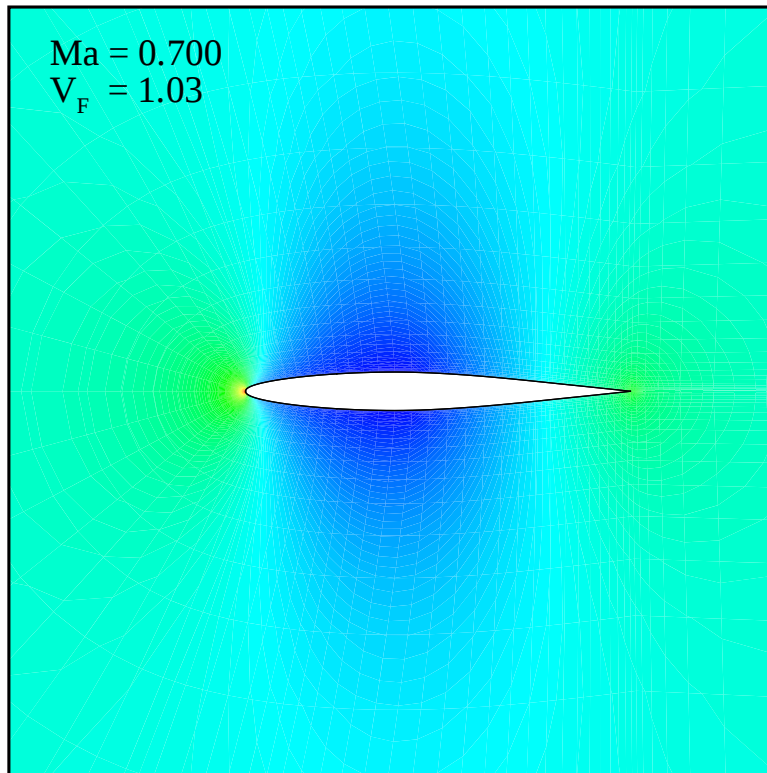
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- ⌞ Motivation
- ⌞ Bifurcation approach and BIFOR Solver
- ⌞ Oscillatory Instability Boundary
- ⌞ Conclusion

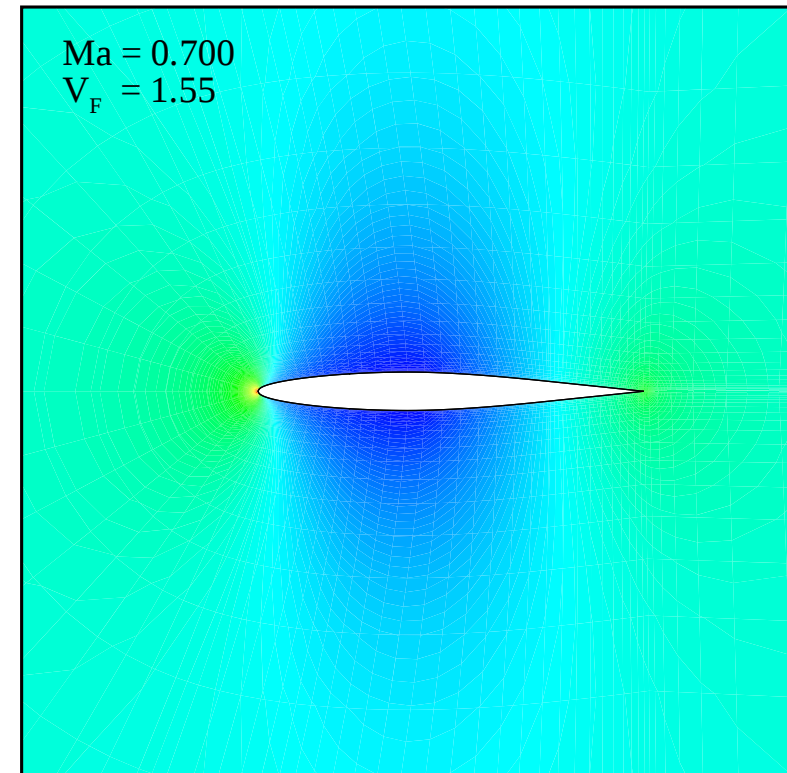
Motivation

- Benchmark case of Isogai, NACA 64A010 aerofoil at zero angle of attack

Time response to initial disturbance



stable (Ma=0.700, $V_F=1.03$)

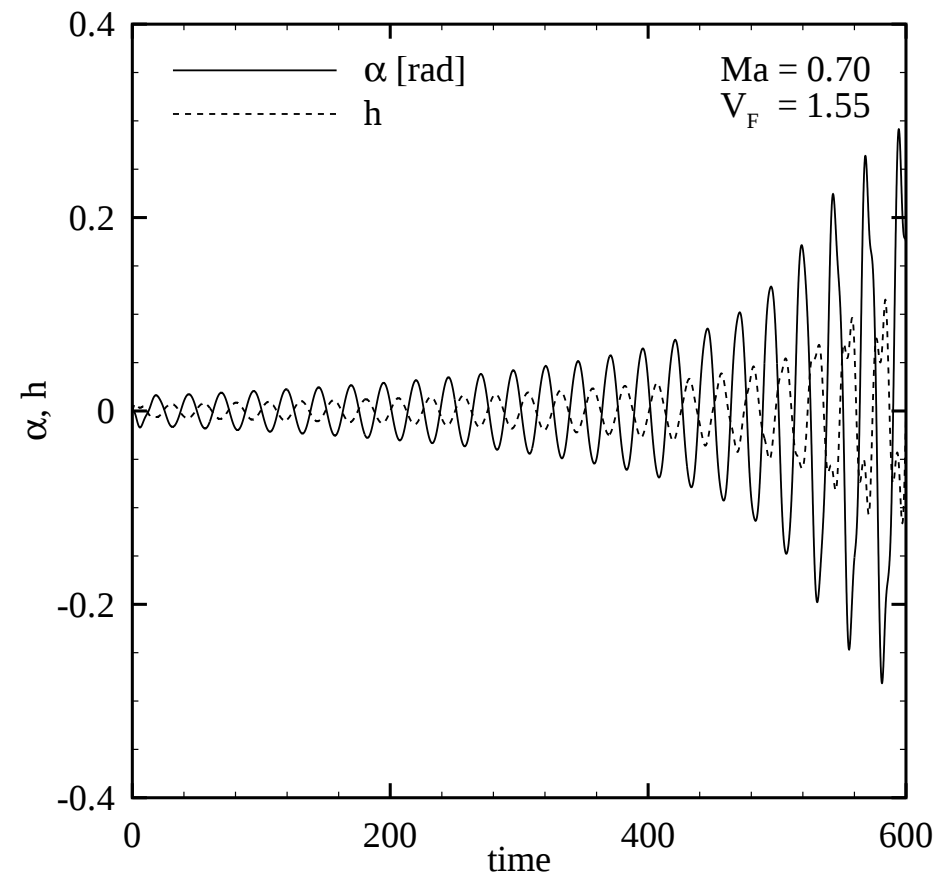
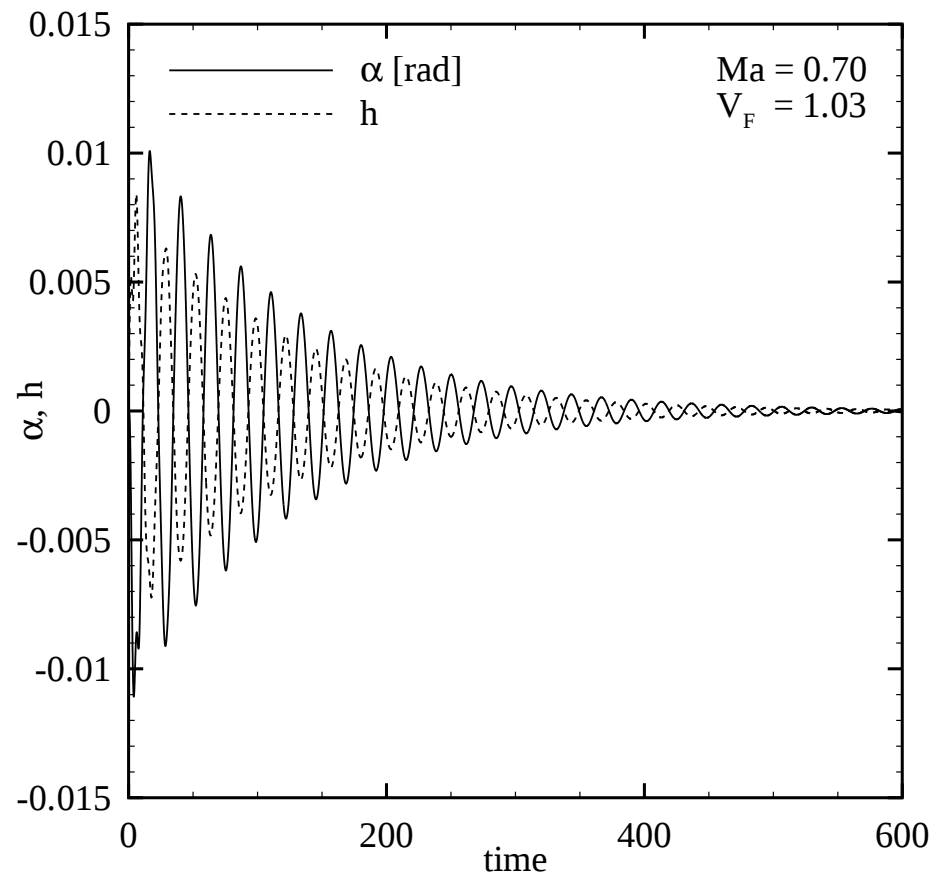


unstable (Ma=0.700, $V_F=1.55$)

[Isogai, AIAA Journal 18 (1981) no. 9, pp. 1240–1242]

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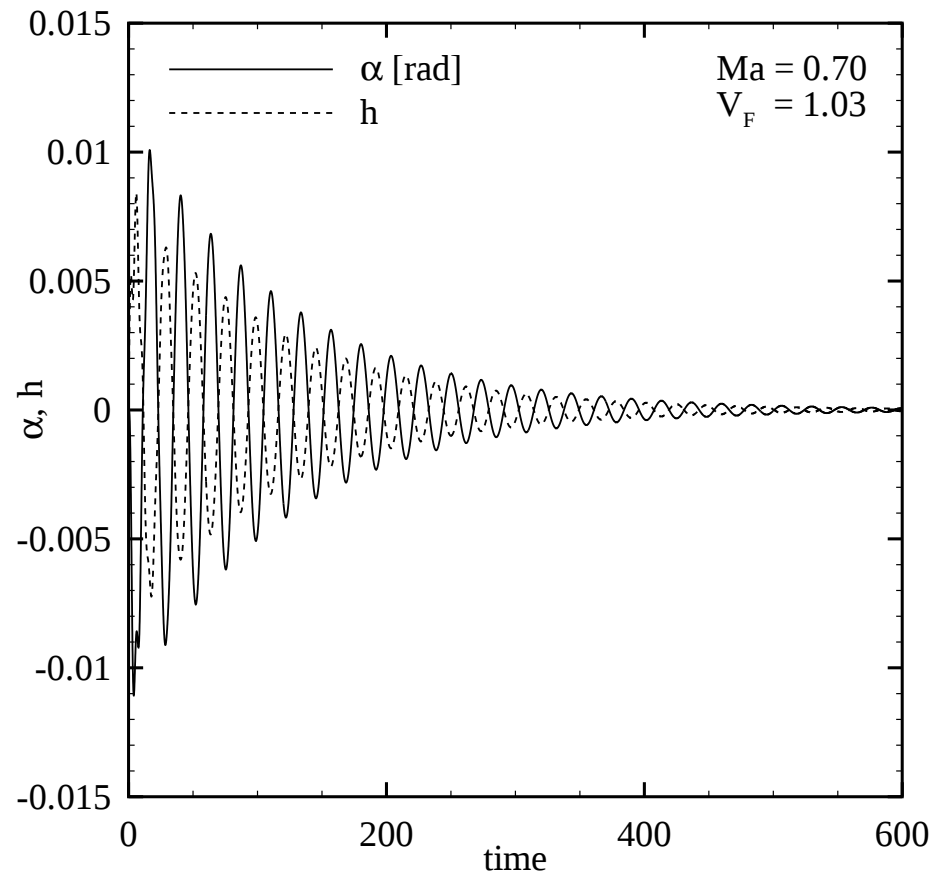
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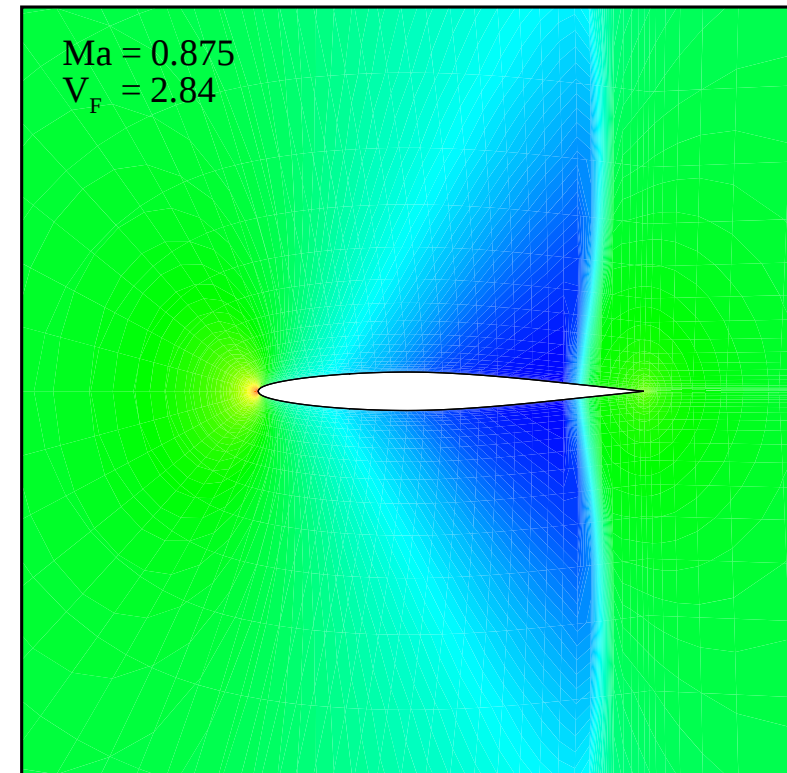
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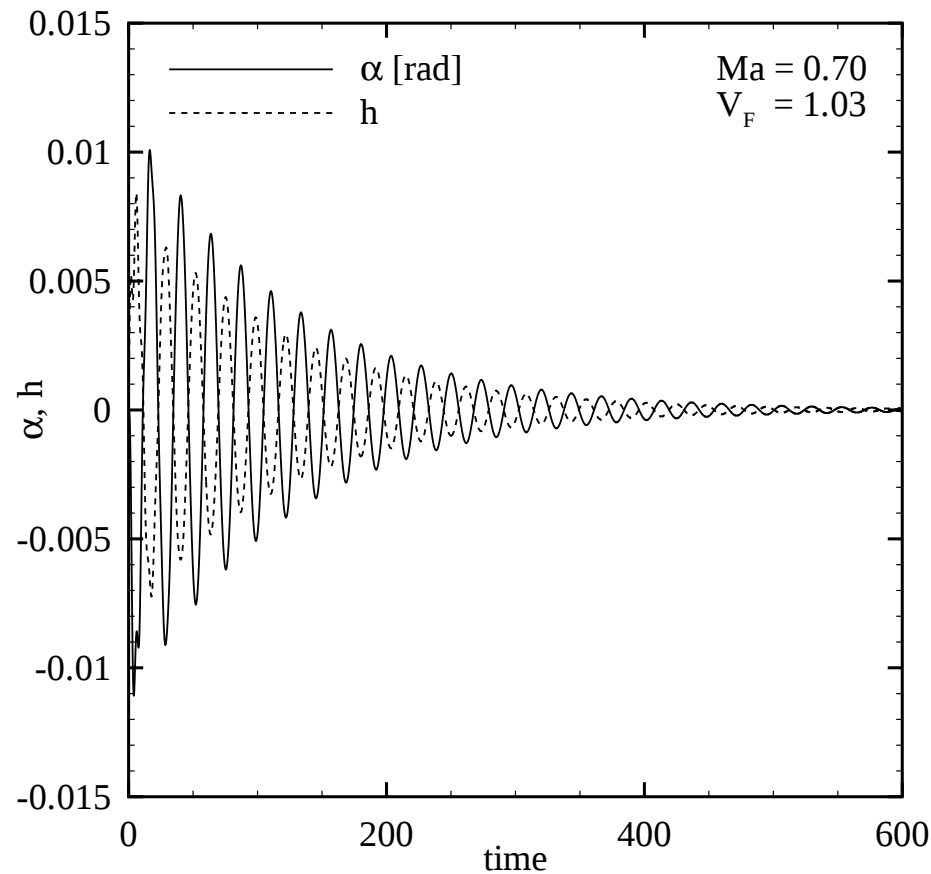


unstable ($Ma=0.875$, $V_F=2.84$)

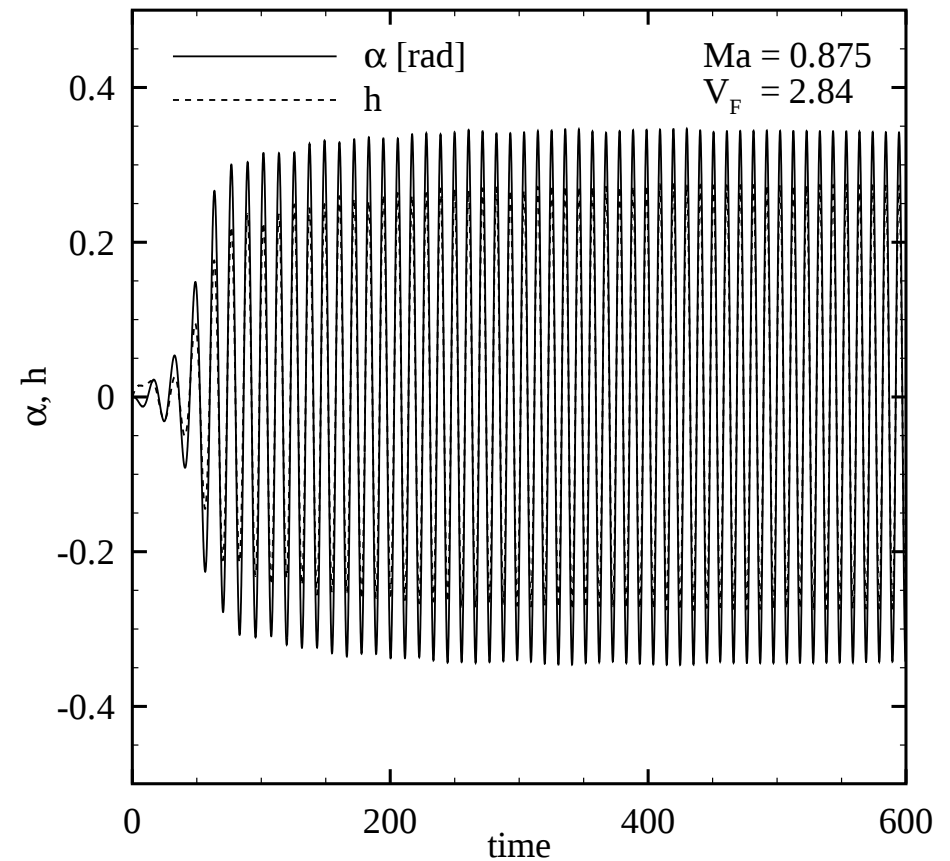
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BIFOR Solver

- Coupled full-order fluid/structure solver
- Three main parts:
 - Steady state solver (Euler, Euler/BL and Full Potential)
 - Eigenvalue solver (shifted inverse power method algorithm, Newton eigenvalue solver)
 - Unsteady time-accurate solver

- Coupled full-order fluid/structure solver
- Three main parts
- Steady state solver (Euler):
 - Implicit time marching
 - Osher's approximate Riemann solver
 - MUSCL variable extrapolation and van Albada's limiter
 - Preconditioned Krylov subspace method
 - Applied within pseudo-time iterations in unsteady calculations

[Badcock et al, Progress in Aerospace Sciences 36 (2000), pp. 351–392]

- Coupled full-order fluid/structure solver
- Three main parts
- Steady state solver
- Consider coupled fluid-structure system $\Rightarrow \frac{d\mathbf{w}}{dt} = \mathbf{R}(\mathbf{w}(\mu), \mu)$
- Equilibrium $\mathbf{w}_0$ given by $\Rightarrow \mathbf{R}(\mathbf{w}_0(\mu), \mu) = 0$
 - Shock nonlinearity (location and strength) defined in steady flow field

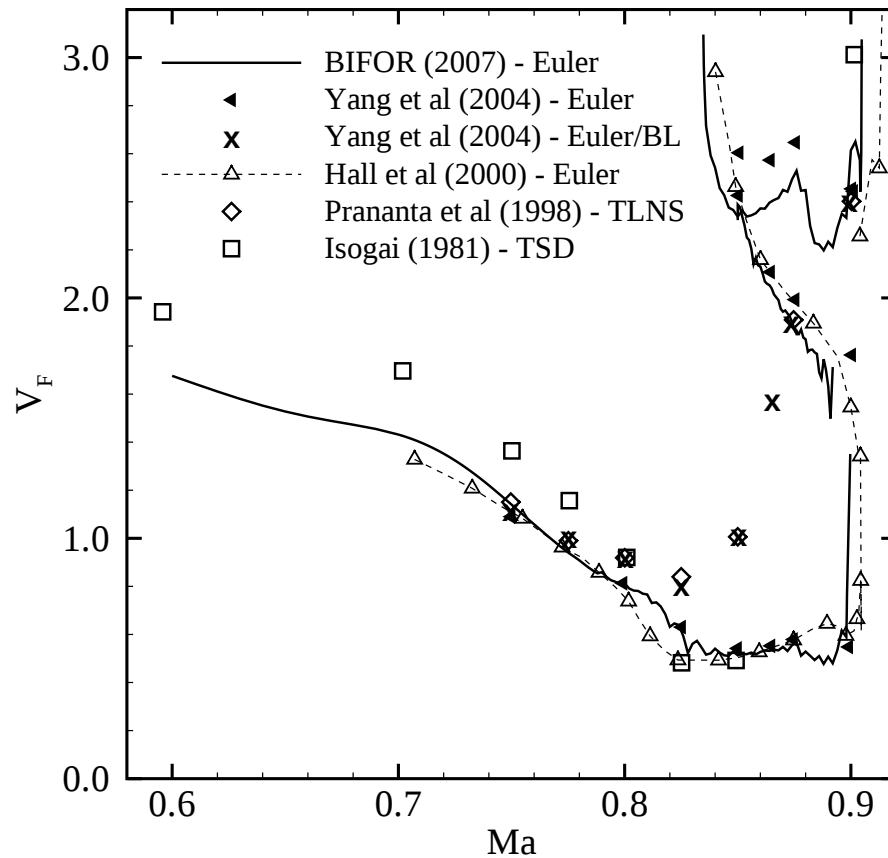
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- Stability determined by eigenvalues $\lambda_j = \gamma_j \pm i\omega_j$ of Jacobian $\Rightarrow A(\mathbf{w}_0, \mu) = \frac{\partial \mathbf{R}}{\partial \mathbf{w}}$
 - Small number of eigenvalues associated with loss of stability
 - Dynamics of system dominated by evolution of these critical modes

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- Extended eigenvalue problem $\Rightarrow \mathbf{R}_{EV}(\lambda, \mathbf{p}) = \begin{bmatrix} (A - \lambda I) \mathbf{p} \\ \mathbf{q}_s^T \mathbf{p} - i \end{bmatrix} = 0$

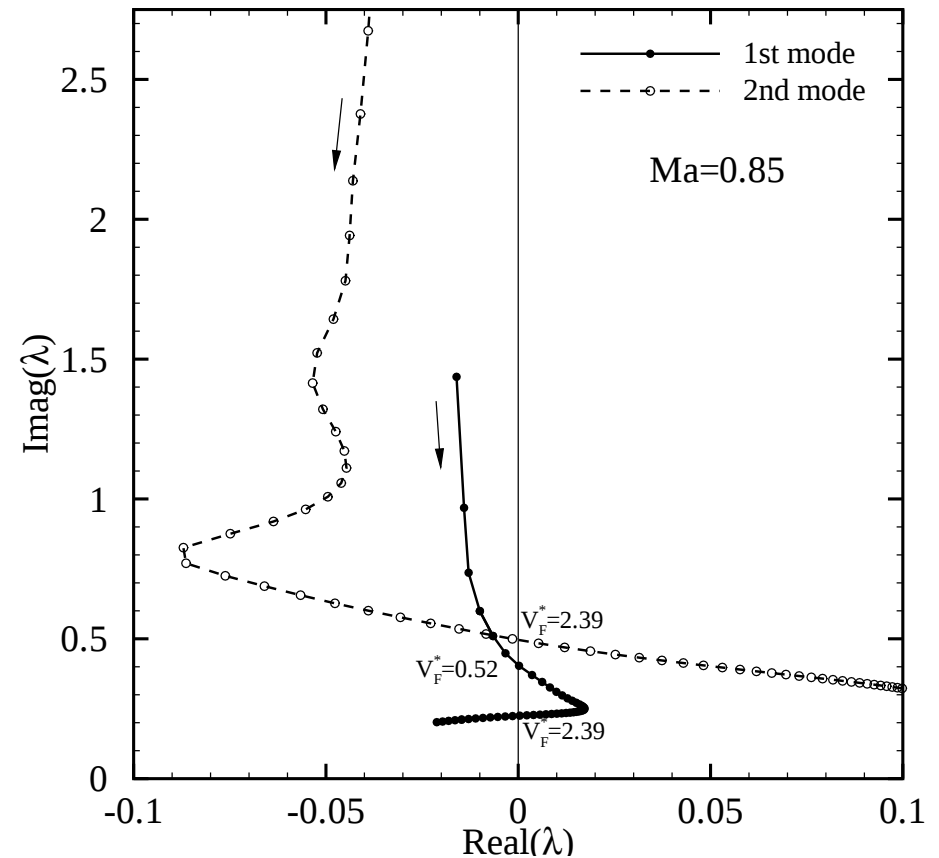
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- BIFOR solver used for two tasks
 - Tracking of aeroelastic modes $\Rightarrow \lambda_j = \lambda_j(\mu) = \gamma_j \pm i\omega_j$
 - Detecting of instability point $\Rightarrow \lambda_j = \pm i\omega_j$ for $\mu = \mu^*$

- Benchmark case of Isogai, NACA 64A010 aerofoil at zero angle of attack

Highly-resolved transonic instability boundary



Instability boundary



Root loci

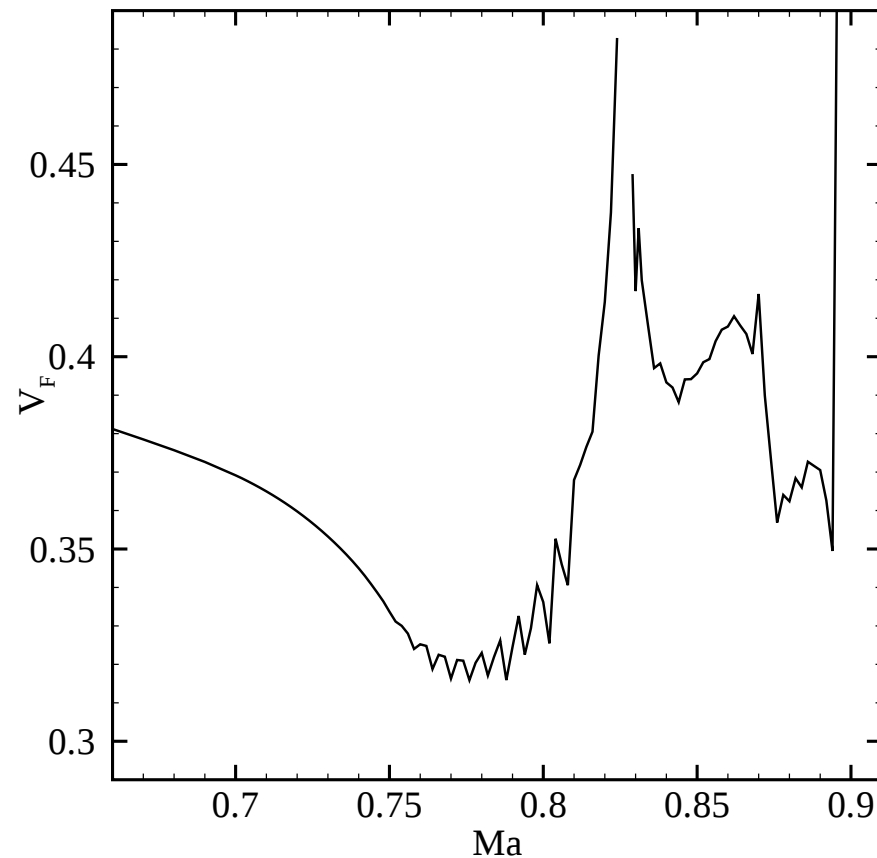
Computational costs

Grid dimension	Steady state solver (CFL=100, conv.=1.e-10)	Eigenvalue solver ($\gamma_j=1.e-07$)	Unsteady solver ($\Delta t=0.05$, $N_{\text{step}}=6.e+06$)
129 × 33 (4.2k)	6 s	70 s	7 h
257 × 65 (16.7k)	60 s	600 s	30 h
513 × 65 (33.3k)	250 s	1700 s	—

Oscillatory Instability Boundary

- Oscillatory behaviour observed for transonic flow condition ($Ma > Ma^*$)

NACA 0012



Instability boundary

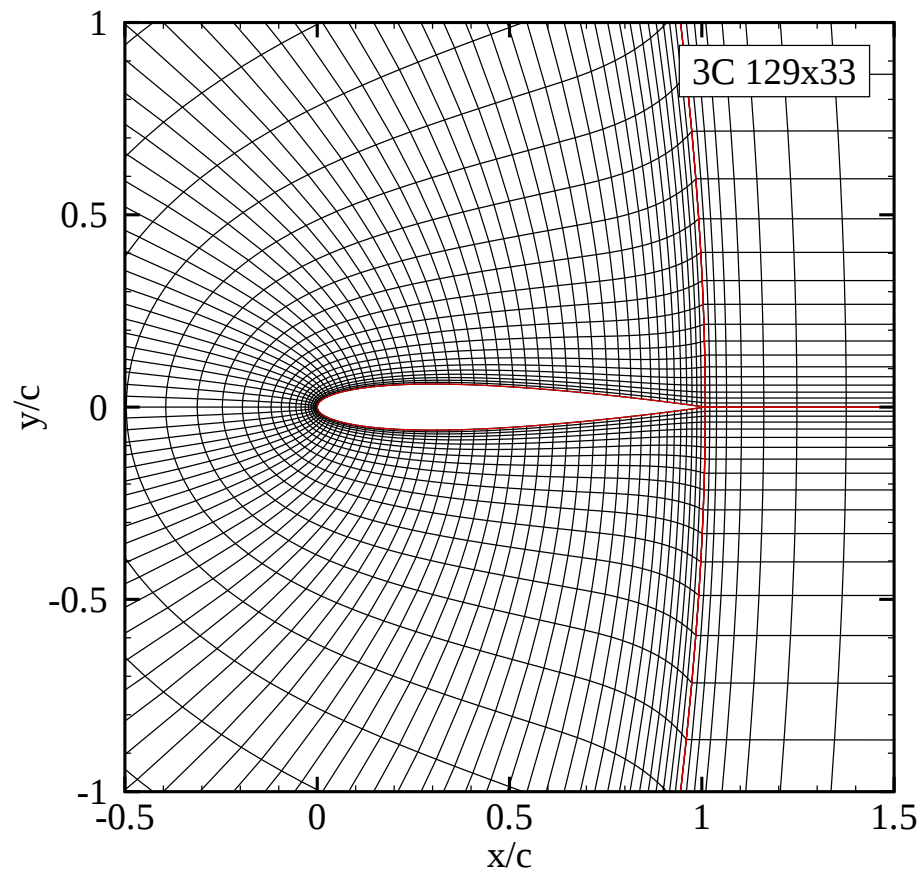
Structural parameter

- aerofoil-to-fluid-mass ratio $\mu_s = 100$
- ratio of natural frequencies $\omega_r = 0.343$
- radius of gyration $r_\alpha = 0.539$
- center of gravity $x_{cg} = 0.5$
- static unbalance $x_\alpha = -0.2$

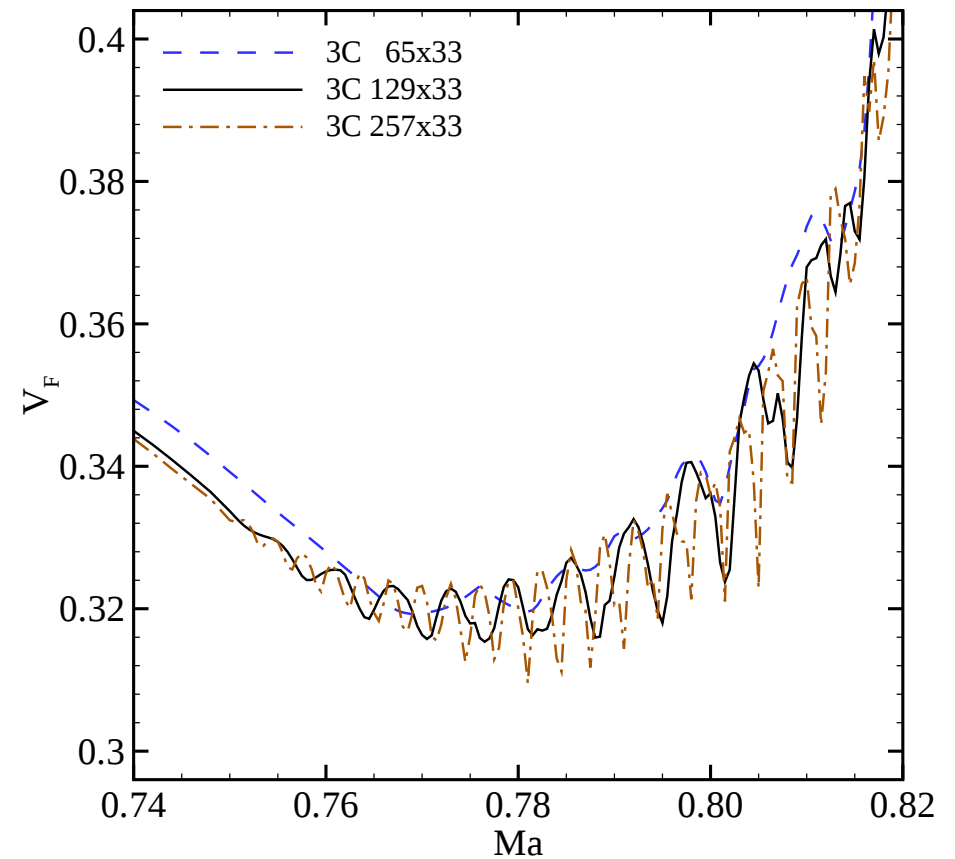
[Badcock et al, AIAA Journal 42 (2004) no. 5, pp. 883–892]

✧ NACA 0012 at zero angle of attack

3 block, C-type grid



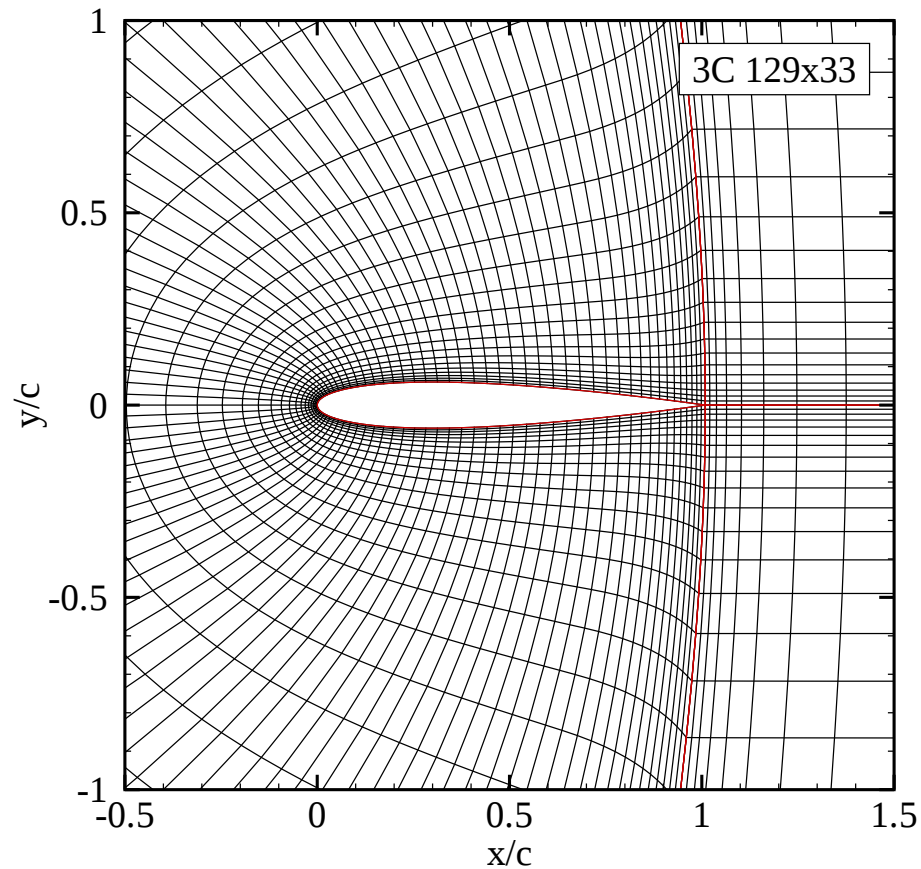
Grid topology



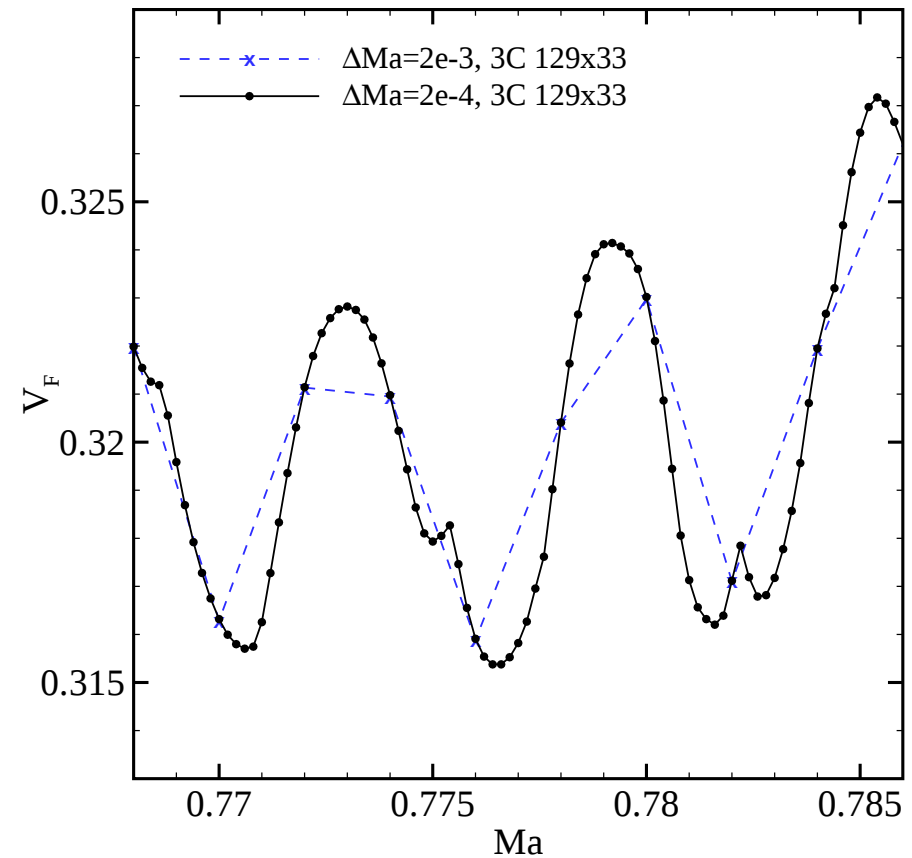
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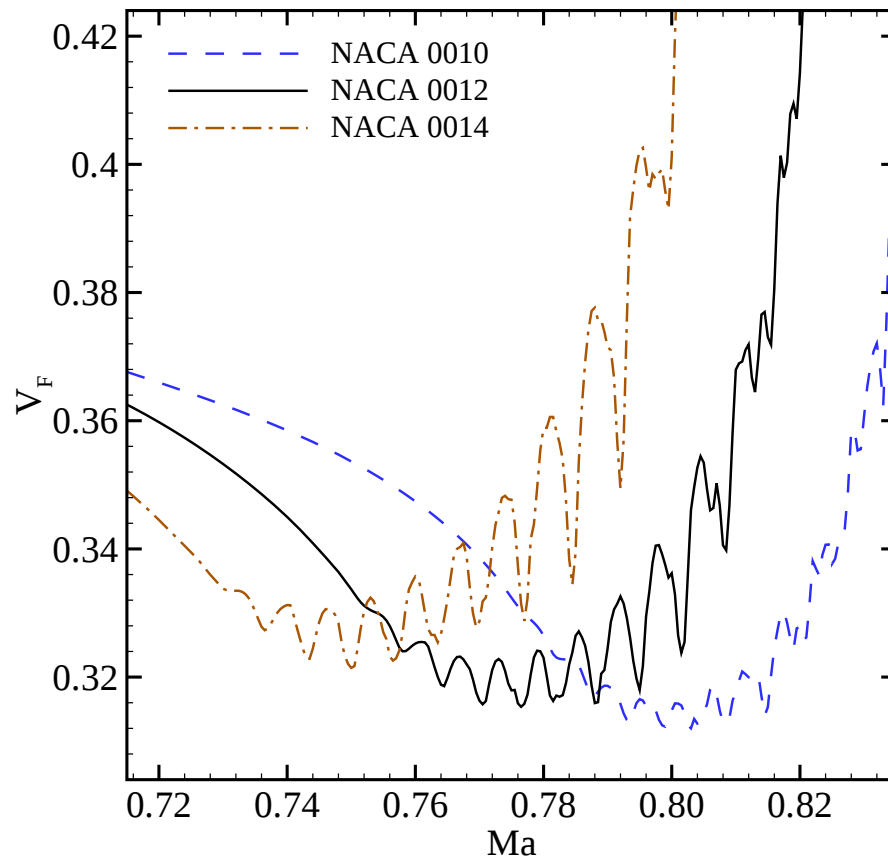
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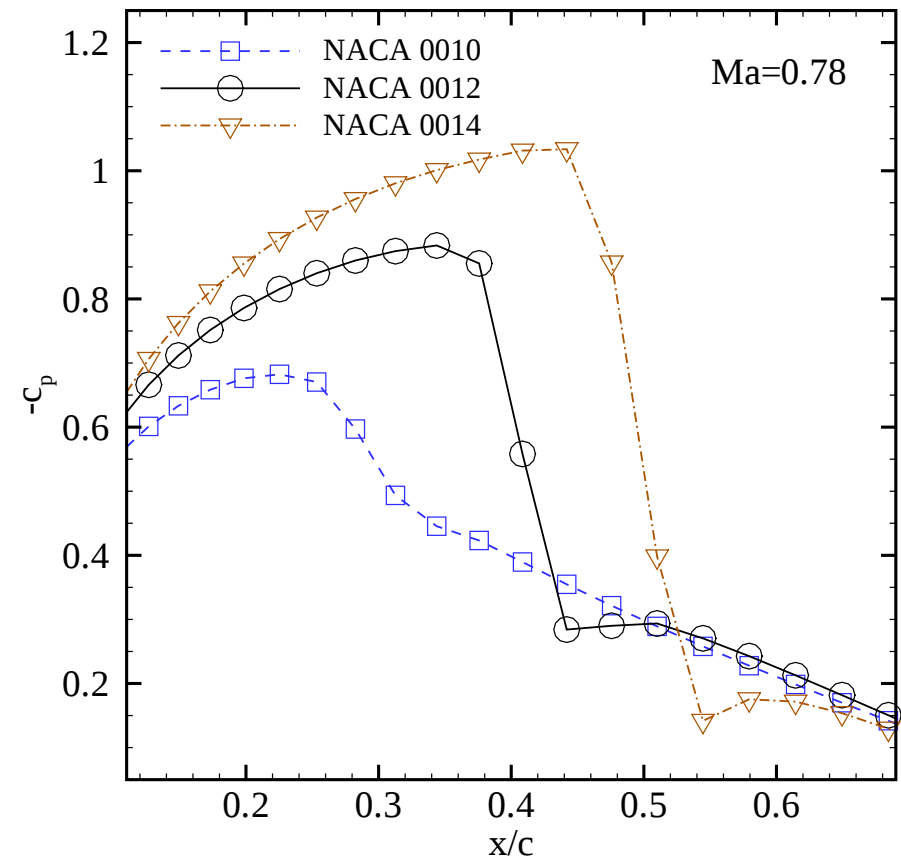
Instability boundary

✧ NACA 00xx at zero angle of attack

3 block, C-type grid



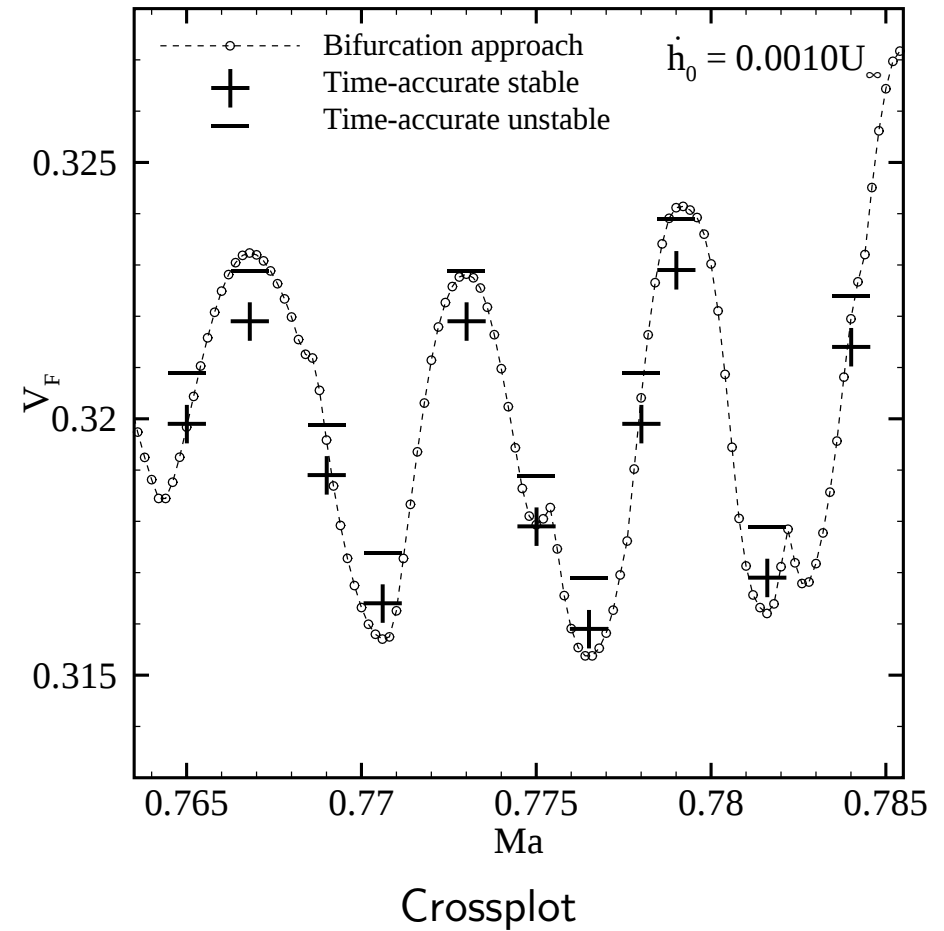
Grid topology



Instability boundary

➤ Time-accurate results crossplotted with bifurcation results

- Time-response due to initial disturbance
- Plunge rate disturbed by $\dot{h}_0 = 0.001U_\infty$



➤ Resolution of shock wave

Shock wave physically

- Event of very limited spatial extent
- Thickness of normal shock front of order

$$\delta x \approx 5.E-08c$$

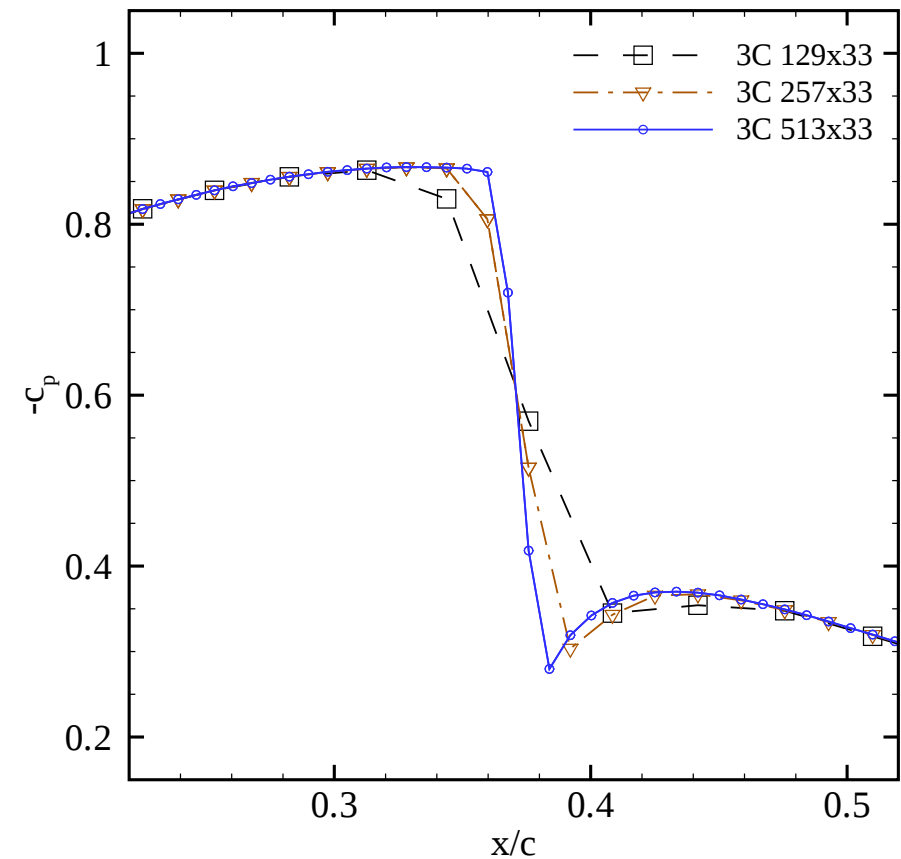
[Granger, *Fluid Mechanics*, Holt, Rinehart & Winston]

Shock wave numerically

- Resolved thickness dependent on grid spacing

$$\Delta x_{\text{grid}} \approx 1.E-02c$$

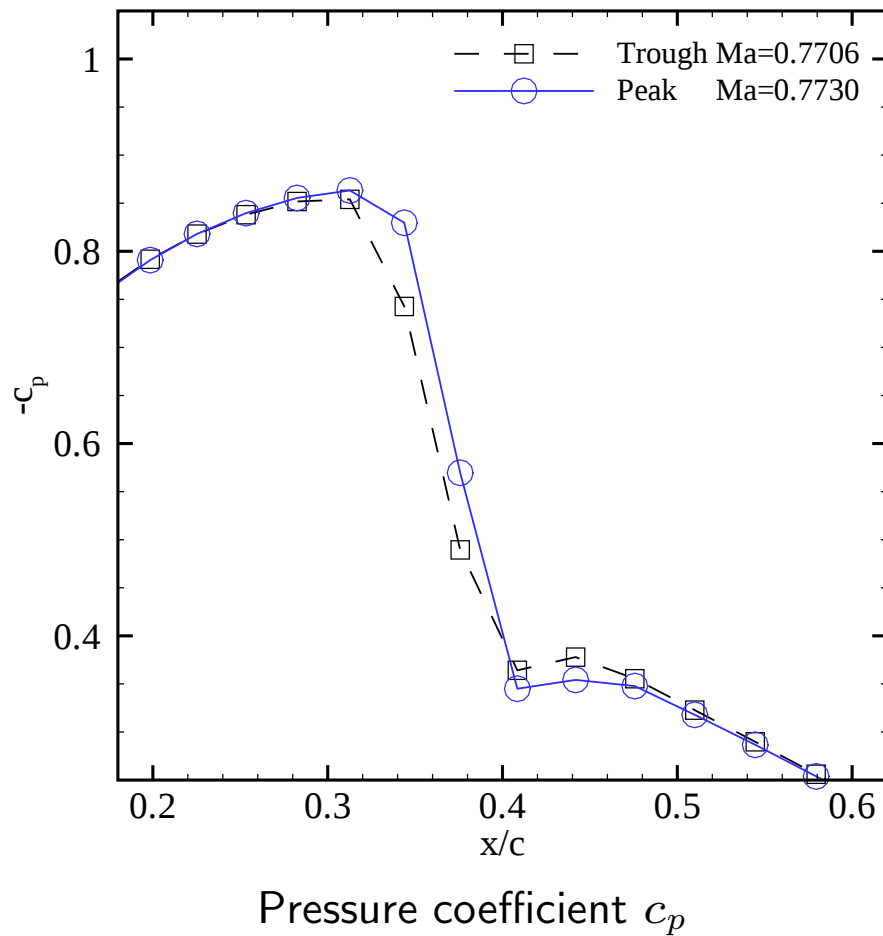
- Two grids points best possible



Pressure coefficient (Ma=0.773)

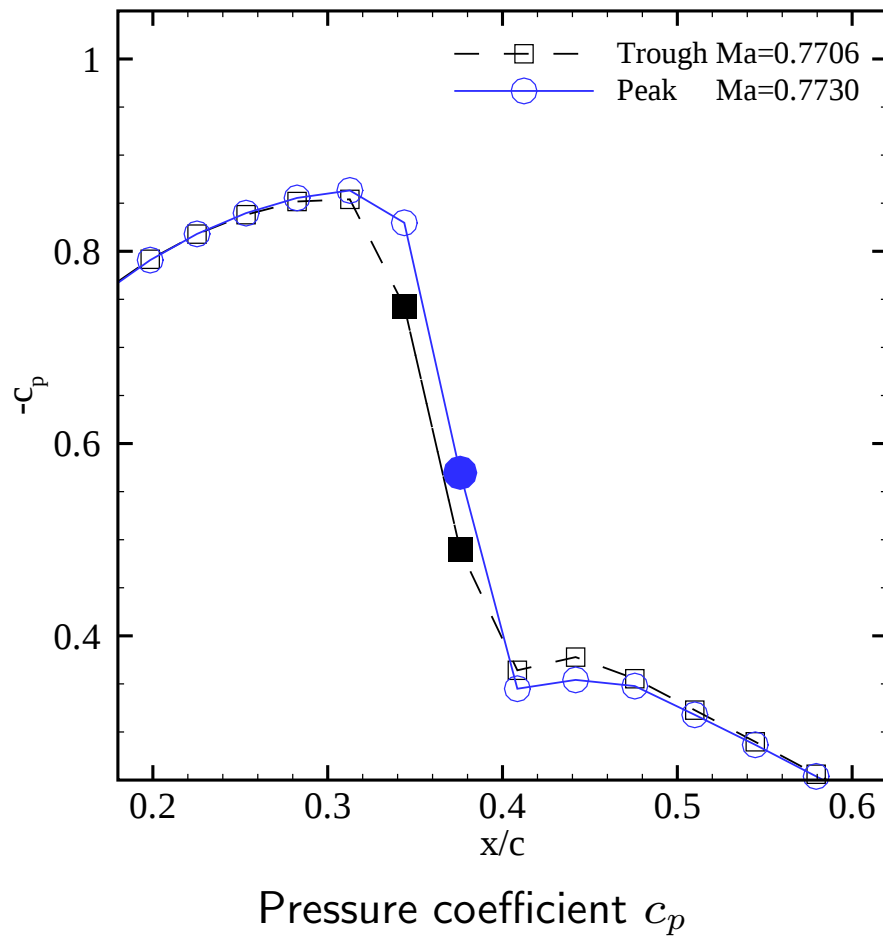
➤ Resolution of shock wave

Steady state results at two Mach numbers (3C 129x33)



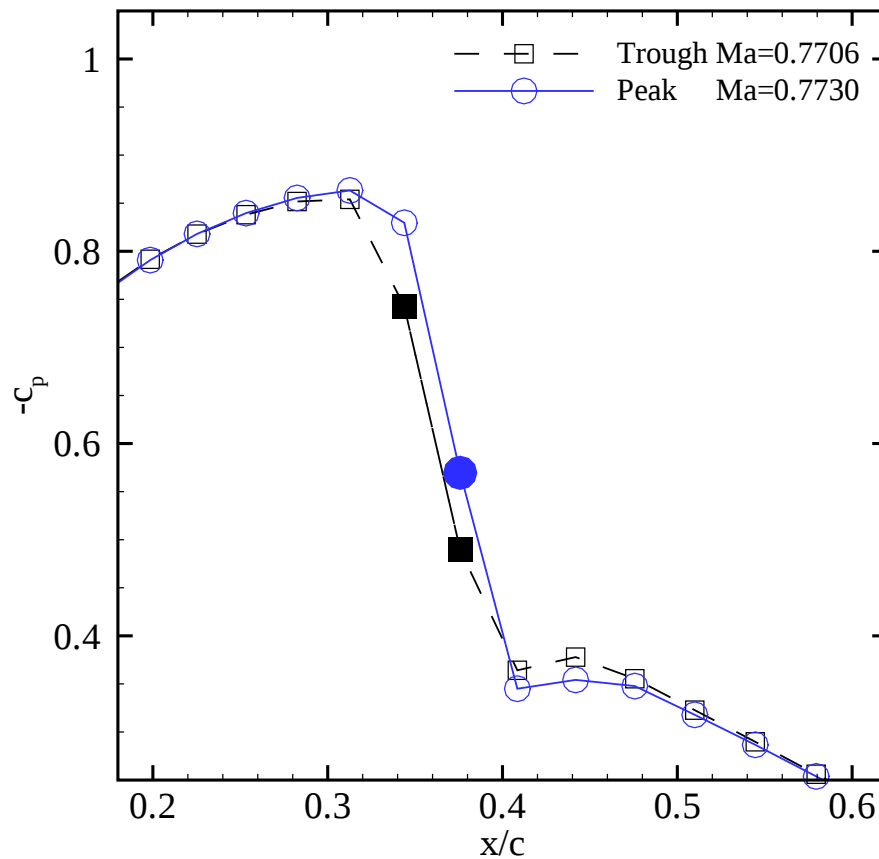
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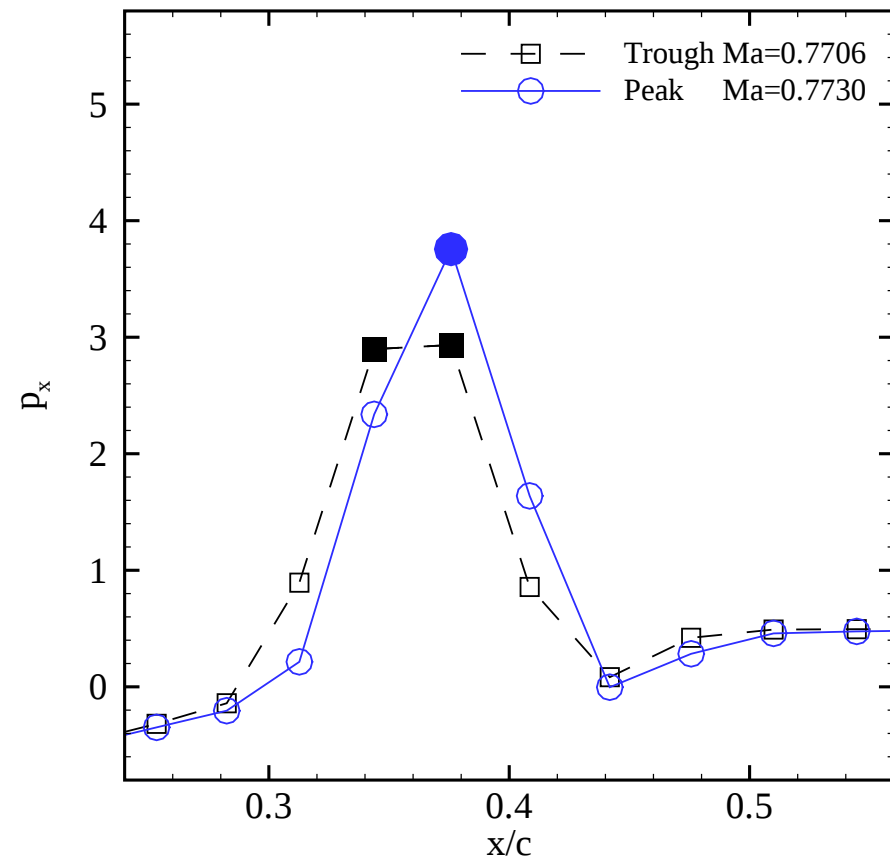


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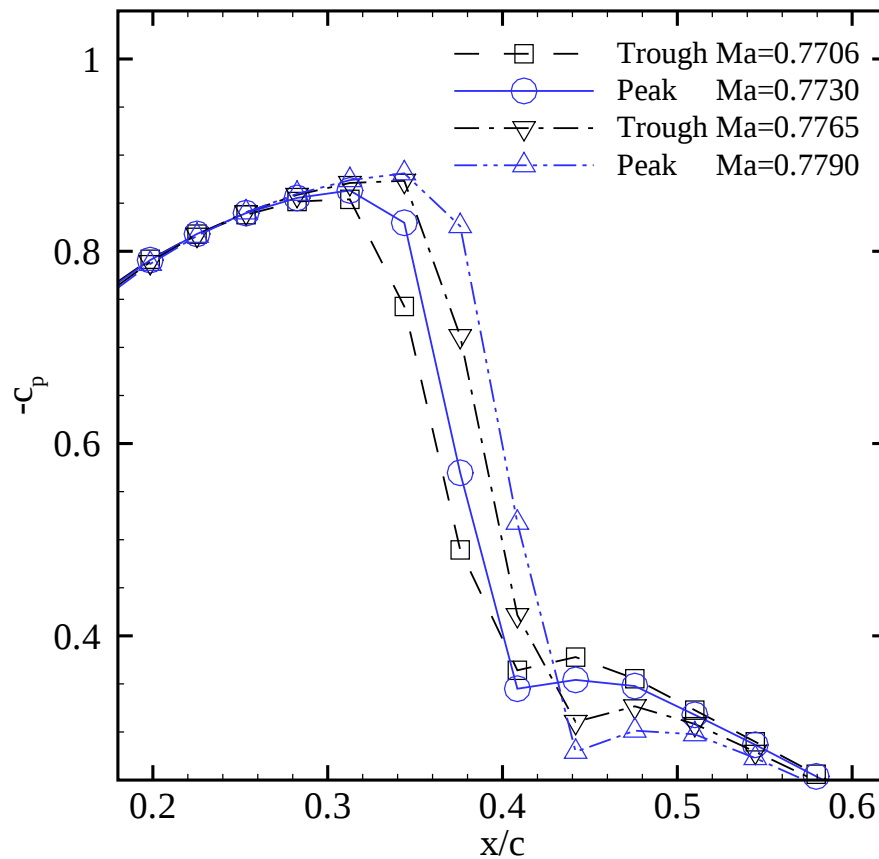
Pressure coefficient c_p



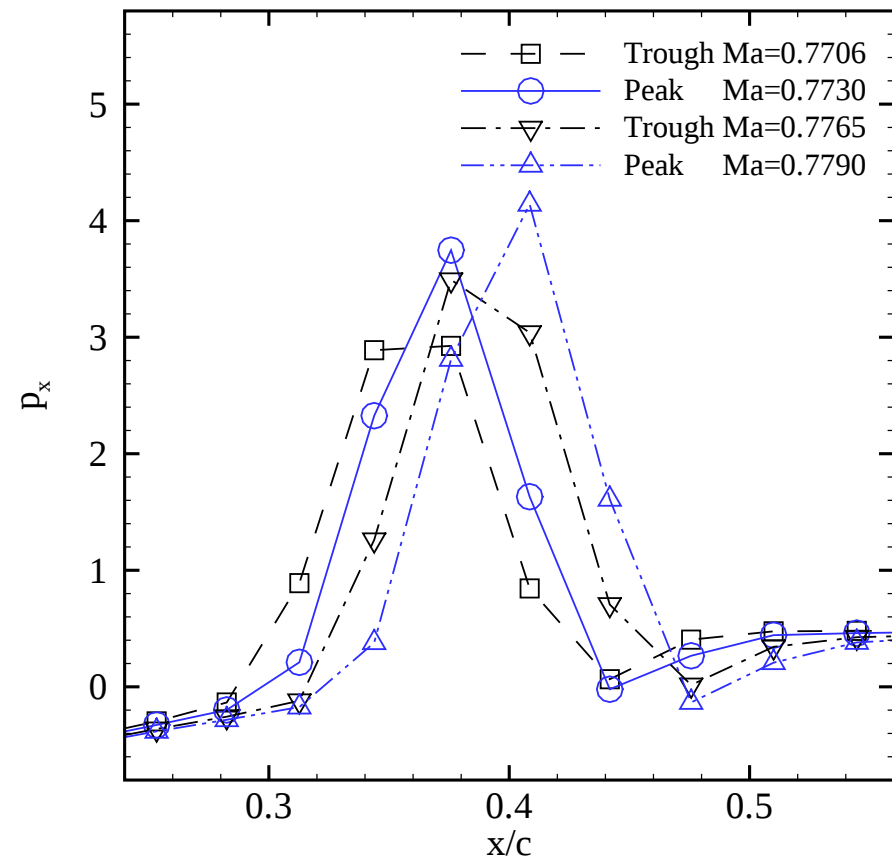
Pressure change $\partial p / \partial x$

Resolution of shock wave

Steady state results at four Mach numbers (3C 129x33)



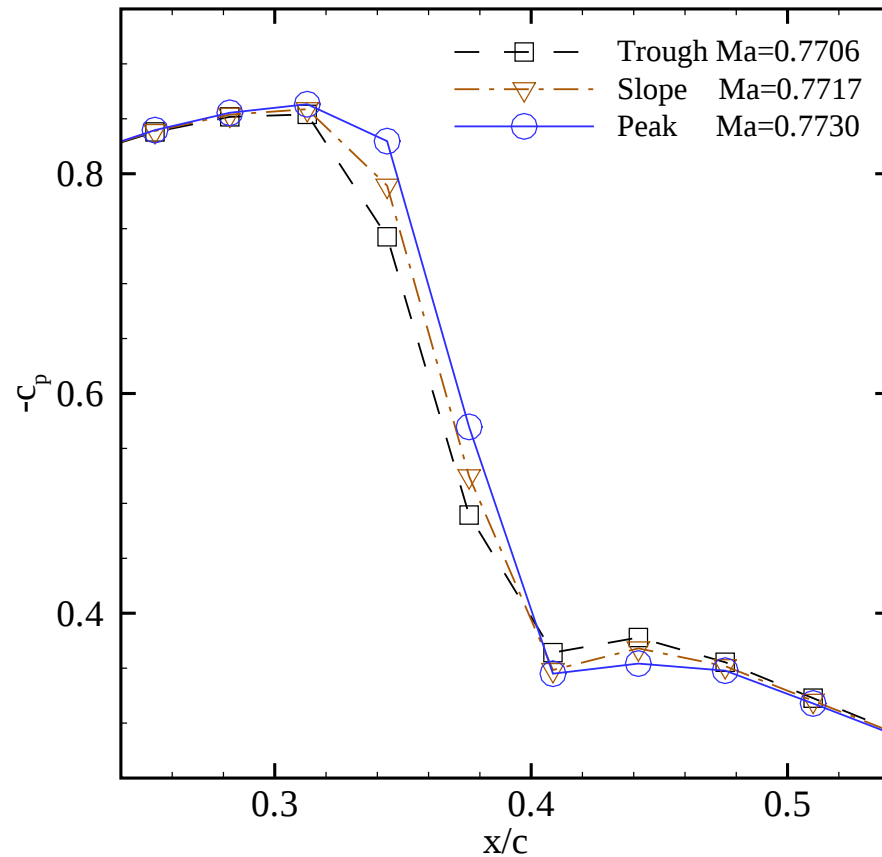
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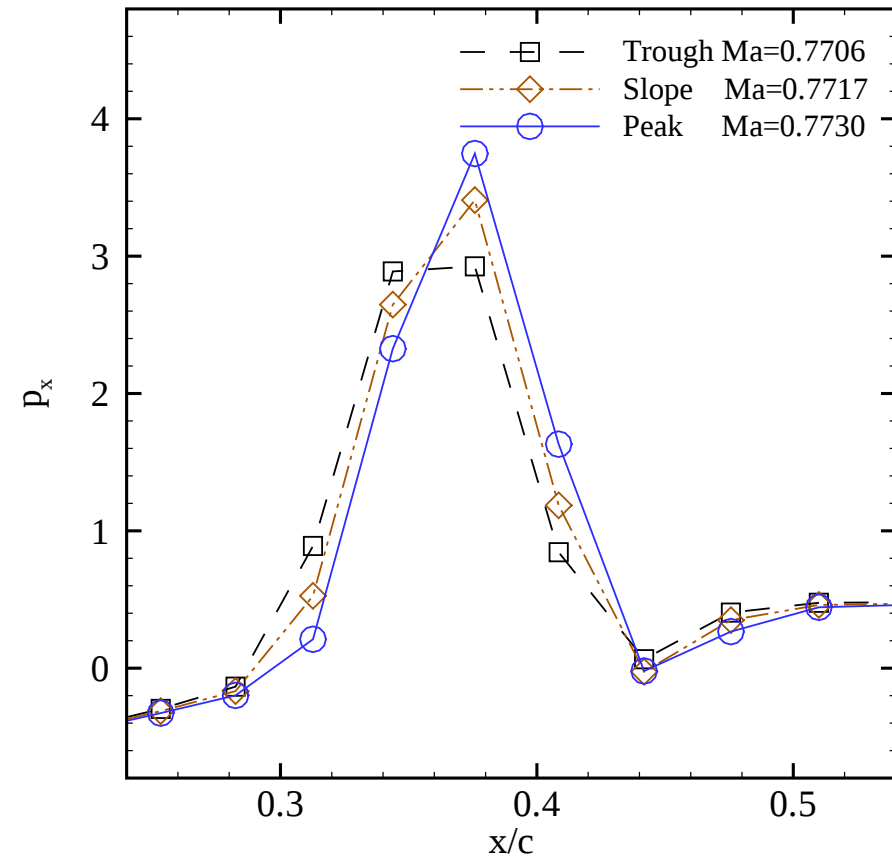
Pressure change $\partial p / \partial x$

➤ Resolution of shock wave

Steady state results at three Mach numbers (3C 129x33)



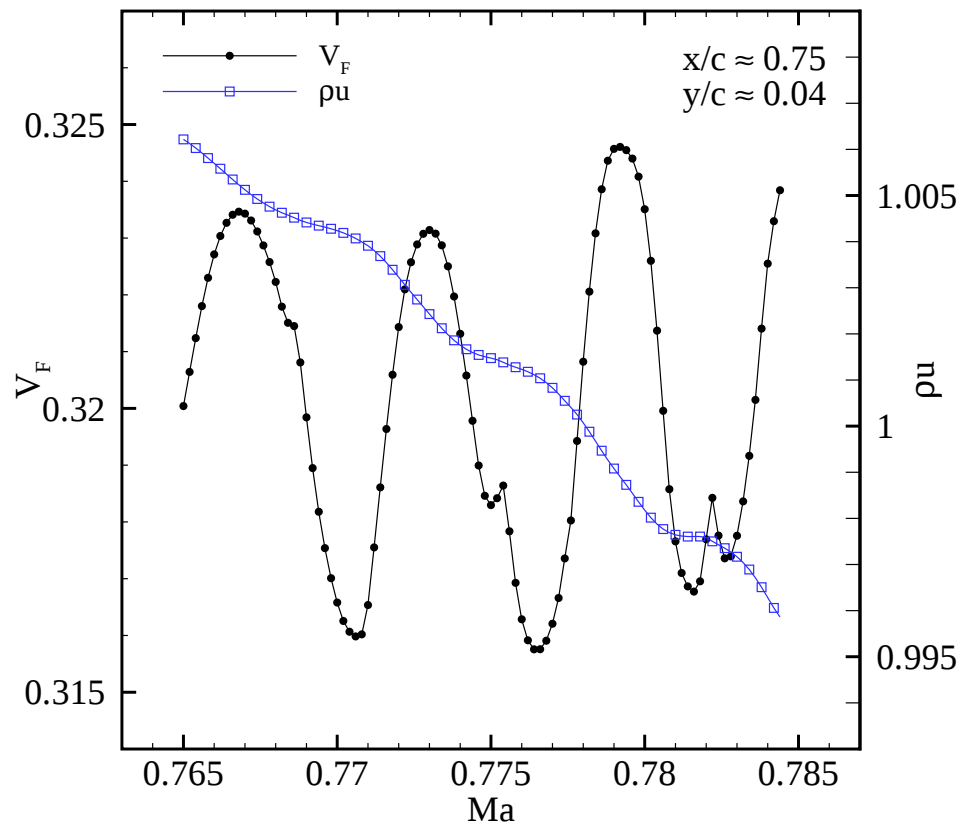
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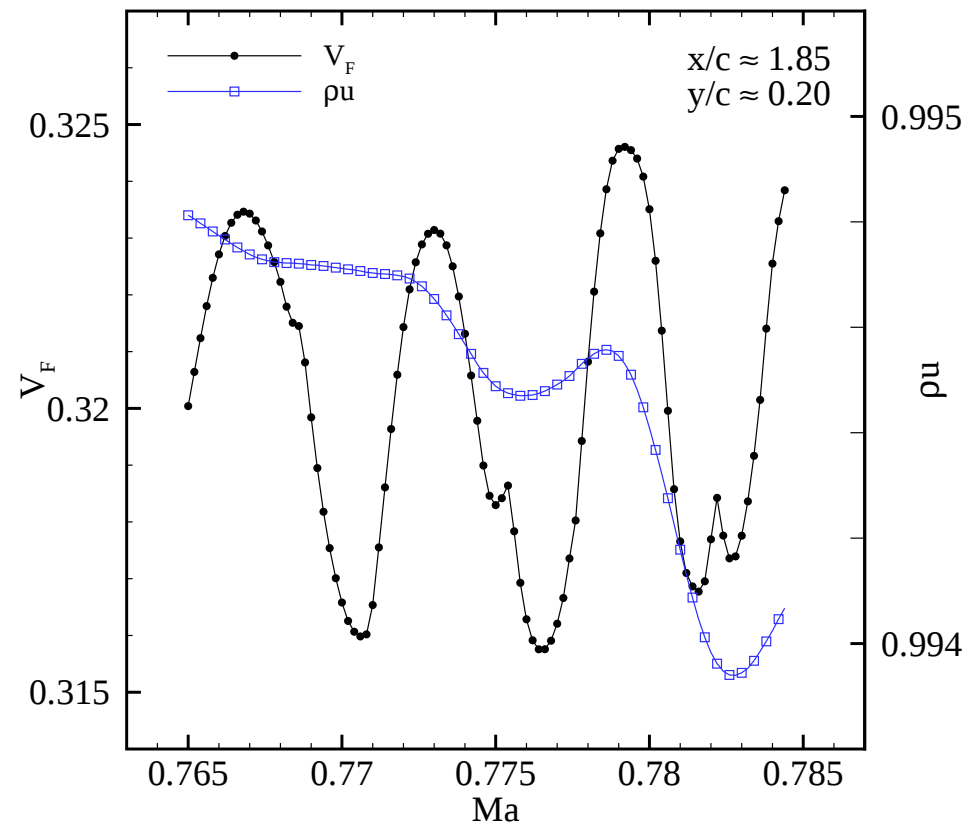
Pressure change $\partial p / \partial x$

- Resolution of shock wave perceived in flow field

Crossplots of instability boundary and steady state results (3C 129x33)



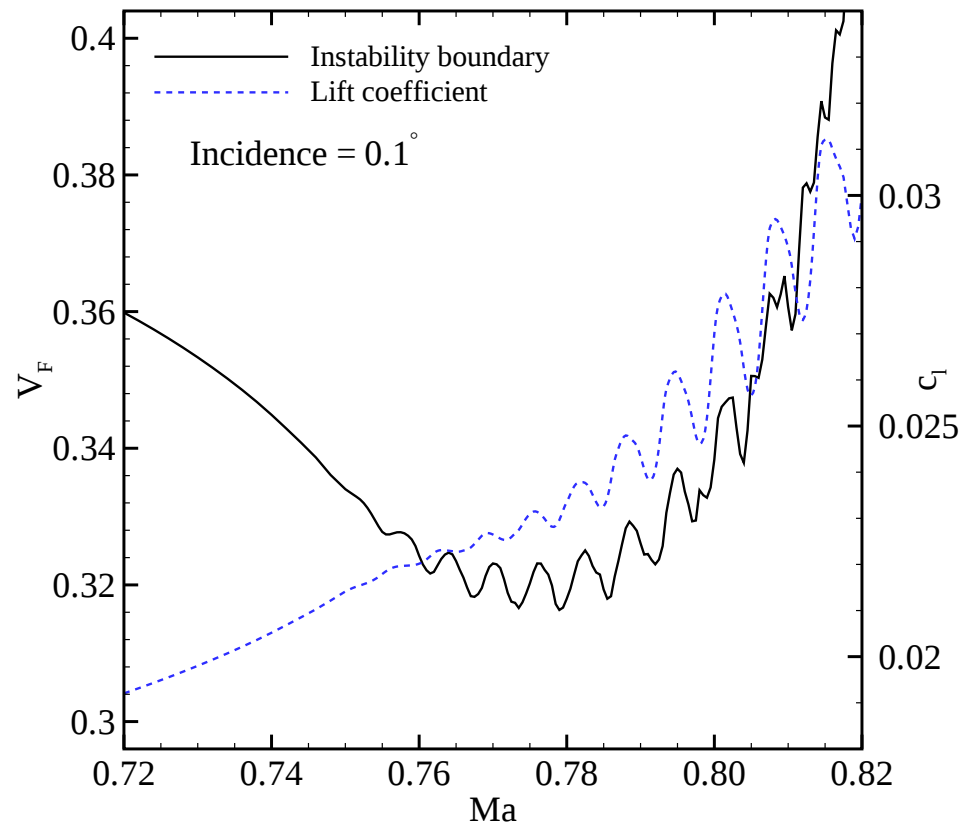
Aerofoil location ($x/c \approx 0.75$, $y/c \approx 0.04$)



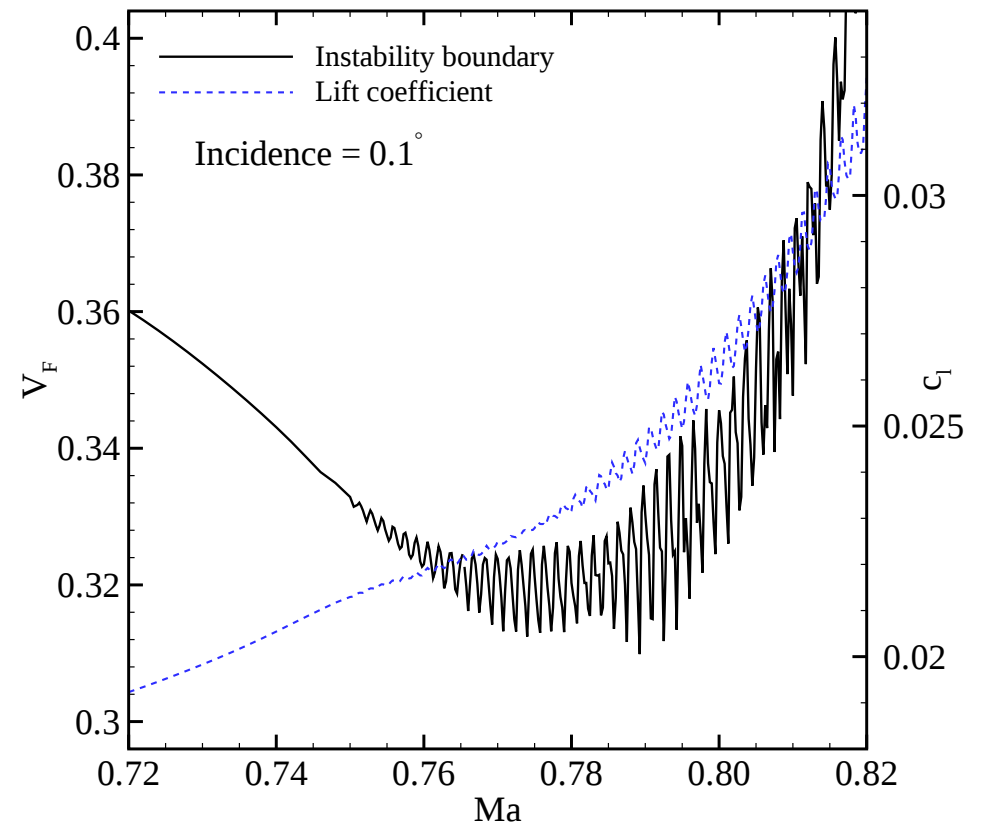
Wake location ($x/c \approx 1.85$, $y/c \approx 0.20$)

- Resolution of shock wave perceived in flow field

Crossplots of instability boundary and lift coefficient



3C 129x33



3C 513x33

Conclusion

- Bifurcation method using full-order nonlinear aerodynamics
- Efficient simulation of aeroelastic instabilities

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- Efficient simulation of aeroelastic instabilities

* * *

- High resolution of instability boundary revealed oscillatory behaviour
- Numerical artefact due to shock wave resolution

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